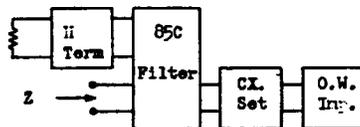


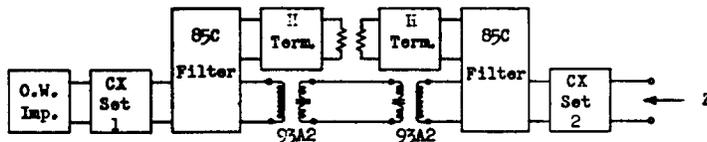
Intermediate Equipment Return Loss

85C (86A) Filter



Freq.	104-Mil Copper - 12" Spacing							
	Side				Phantom			
	CX		No CX		CX		No CX	
	Z	R.L.	Z	R.L.	Z	R.L.	Z	R.L.
200	-	-	707/55.6	14	1037/29.8	11	623/51.7	30
300	652/49.8	12	577/29.9	13	729/34.2	14	536/25.9	33
500	413/23.3	11	502/9.1	13	554/29.1	17	476/16.9	32
1000	646/20.5	22	679/11.7	13	455/17.6	22	438/10.8	33
1500	905/0	14	865/0	16	421/12.9	25	423/6.4	38
2000	653/15.4	24	607/8.3	33	405/7.1	33	410/1.8	31
2200	562/14.2	21	621/2.6	27	398/4.1	35	405/0	28
2500	613/13.9	15	683/9.4	18	387/0	27	400/2.3	25
2900	813/10.4	16	761/16.3	14	372/5.6	21	397/10.6	19
3000	770/7.0	18	804/10.8	15	374/8.8	19	398/13.6	17
3200	496/4.6	16	500/0	16	372/12.4	17	401/17.6	15

Freq.	120-Mil Copper - 12" Spacing			
	Side			
	CX		No CX	
	Z	R.L.	Z	R.L.
200	-	-	690/1.0	17
300	596/3.1	13	574/20.0	16
500	418/16.6	12	541/4.0	16
1000	692/19.0	12	714/2.1	16
1500	955/1.1	14	626/1.9	16
2000	642/11.3	24	672/4.3	31
2200	573/2.8	25	555/0	29
2500	630/13.7	16	647/6.4	20
2900	702/10.8	16	743/14.2	15
3000	760/8.5	17	705/11.1	16
3200	491/4.7	17	550/0	22

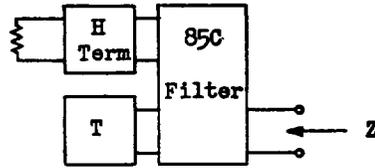


Freq.	104-Mil Copper Side - 12" Spacing					
	No CX		CX 1		CX 1 and 2	
	Z	R.L.	Z	R.L.	Z	R.L.
	200	-	-	-	-	-
300	613/37.0	14	623/51.3	11	1200/59.5	10
500	549/6.6	14	455/2.4	10	563/32.5	14
1000	545/11.3	18	582/17.6	20	651/28.3	16
1500	722/18.3	12	758/23.5	11	724/15.1	13
2000	656/7.7	38	603/8.4	26	614/14.2	22
2200	593/0.7	23	603/2.7	21	606/3.8	26
2500	507/5.3	16	495/0	16	487/5.5	17
2900	738/32.9	9	782/29.4	10	775/23.6	11
3000	856/20.7	12	804/17.7	13	767/11.3	15
3200	-	-	-	-	-	-

Freq.	120-Mil Copper Side - 12" Spacing			
	No CX		CX 1	
	Z	R.L.	Z	R.L.
	200	-	-	-
300	626/30.4	18	591/46.4	12
500	589/3.0	20	490/1.5	14
1000	532/9.5	20	569/16.7	20
1500	730/16.5	13	740/21.6	12
2000	609/6.4	30	631/9.1	28
2200	610/1.3	30	610/1.3	26
2500	497/5.4	17	510/0	19
2900	710/30.4	10	727/30.0	10
3000	843/22.3	11	814/21.8	12
3200	-	-	-	-

- Notes:
1. Impedances, Z, were measured on typical installations with the terminations indicated on the sketches and tables. Open wire impedance terminations were precision networks for the type of circuit indicated. The phantom circuit measurements were made on the phantom derived from two side circuit arrangements.
 2. The return losses are between impedance Z and the characteristic impedance of the open wire represented by the termination, or as indicated in case of a more general termination.
 3. For description and uses of the 85C (86A) filter see Section 352-202-100.

SECTION 304-424-100



Sides - 12" Spacing

T =	10 ₄ Imp.		128 Imp.		93A2 Coil + 10 ₄ Imp.		93A2 Coil + 22A1 Repr.						
	Freq.	Z	R.L.	Z	R.L.	Z	R.L.	Z	R.L.	Vs 10 ₄ 128			
200	625	$\sqrt{31.5}$	12	610	$\sqrt{20.9}$	11	970	$\sqrt{50.6}$	16	651	$\sqrt{4.0}$	9	12
300	577	$\sqrt{29.9}$	13	578	$\sqrt{21.0}$	16	712	$\sqrt{41.9}$	15	765	$\sqrt{0.6}$	12	14
500	503	$\sqrt{10.1}$	13	542	$\sqrt{4.7}$	16	502	$\sqrt{20.5}$	14	763	$\sqrt{8.5}$	19	22
1000	674	$\sqrt{8.0}$	15	708	$\sqrt{5.1}$	17	605	$\sqrt{7.1}$	15	603	$\sqrt{6.0}$	21	27
1500	752	$\sqrt{4.4}$	24	718	$\sqrt{6.8}$	25	740	$\sqrt{1.5}$	20	631	$\sqrt{3.5}$	19	22
2000	556	$\sqrt{2.6}$	20	545	$\sqrt{0}$	21	626	$\sqrt{3.5}$	28	691	$\sqrt{2.1}$	22	23
2200	536	$\sqrt{5.9}$	17	545	$\sqrt{8.0}$	18	580	$\sqrt{0}$	21	675	$\sqrt{0}$	26	27
2500	606	$\sqrt{15.0}$	15	640	$\sqrt{14.2}$	15	558	$\sqrt{9.7}$	16	550	$\sqrt{0}$	20	22
2900	636	$\sqrt{15.0}$	15	615	$\sqrt{15.5}$	15	659	$\sqrt{21.1}$	13	766	$\sqrt{34.7}$	9	9
3000	605	$\sqrt{18.2}$	14	590	$\sqrt{20.5}$	13	669	$\sqrt{19.7}$	13	949	$\sqrt{18.5}$	11	11
3200	556	$\sqrt{38.0}$	8	585	$\sqrt{40.8}$	8	555	$\sqrt{40.8}$	7	-	-	-	-

Phantoms - 12" Spacing

T =	10 ₄ Imp.		10 ₄ Imp. + CX on Sides		128 Imp.		128 Imp. + CX on Sides		93B2 Coil + 22A1 Repr.							
	Freq.	Z	R.L.	Z	R.L.	Z	R.L.	Z	R.L.	Z	R.L.	Vs 10 ₄ 128				
200	629	$\sqrt{32.6}$	28	1061	$\sqrt{25.6}$	11	524	$\sqrt{24.9}$	32	866	$\sqrt{32.5}$	11	418	$\sqrt{7.6}$	15	12
300	534	$\sqrt{26.0}$	33	737	$\sqrt{32.8}$	14	472	$\sqrt{19.2}$	32	634	$\sqrt{32.8}$	14	486	$\sqrt{1.8}$	14	12
500	470	$\sqrt{18.7}$	34	558	$\sqrt{28.6}$	17	438	$\sqrt{13.2}$	32	499	$\sqrt{25.4}$	17	526	$\sqrt{2.7}$	15	14
1000	433	$\sqrt{10.9}$	34	463	$\sqrt{18.3}$	21	418	$\sqrt{6.9}$	33	437	$\sqrt{15.8}$	21	538	$\sqrt{0.3}$	16	16
1500	422	$\sqrt{6.4}$	39	433	$\sqrt{13.9}$	23	410	$\sqrt{3.9}$	35	412	$\sqrt{10.5}$	25	526	$\sqrt{2.1}$	16	17
2000	410	$\sqrt{1.8}$	31	407	$\sqrt{7.1}$	34	400	$\sqrt{0.4}$	31	392	$\sqrt{5.6}$	34	521	$\sqrt{5.5}$	16	16
2200	404	$\sqrt{0}$	28	402	$\sqrt{5.8}$	36	395	$\sqrt{0}$	31	390	$\sqrt{4.1}$	38	520	$\sqrt{9.2}$	15	15
2500	388	$\sqrt{4.1}$	22	390	$\sqrt{0}$	27	393	$\sqrt{6.9}$	21	380	$\sqrt{0}$	30	566	$\sqrt{16.1}$	12	12
2900	386	$\sqrt{10.9}$	18	378	$\sqrt{2.7}$	23	387	$\sqrt{10.9}$	18	373	$\sqrt{8.5}$	20	746	$\sqrt{11.3}$	10	10
3000	387	$\sqrt{14.1}$	16	379	$\sqrt{8.7}$	19	389	$\sqrt{14.0}$	16	370	$\sqrt{11.7}$	17	765	$\sqrt{7.0}$	10	10
3200	399	$\sqrt{17.7}$	15	379	$\sqrt{12.2}$	16	389	$\sqrt{18.1}$	15	369	$\sqrt{15.7}$	15	710	$\sqrt{0}$	11	11